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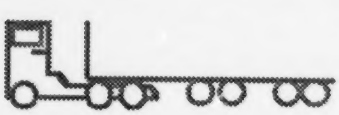
Demonstration of Tractor-Trailer Performance: 6-Axle 48 ft Semi



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Demonstration of Tractor-Trailer Performance: 6-Axle 48 ft Semi

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Abstract:
A 6-axle 48 ft (14.63 m) semitrailer combination was tested by the Ontario Ministry of Transportation and Communications (MTC) as part of the CCMTA/RTAC Vehicle Weight and Dimensions Study. The vehicle was designated an additional vehicle by the study.

The vehicle was subjected to turning, air brake system, lateral/directional and roll stability, and trailer sway tests. A demonstration of straight-line braking was also conducted. Tests were conducted with the empty vehicle on a low-friction surface and the loaded vehicle on a high-friction surface.

This report presents detailed results of the tests and demonstrations.

Key Words: truck testing, offtracking, truck turning, air brake system, braking, truck dynamic tests, rearward amplification, rollover, lane change, tilt test

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ABSTRACT

A 6-axle 48 ft (14.63 m) semitrailer combination was tested by the Ontario Ministry of Transportation and Communications (MTC) as part of the CCMTA/RTAC Vehicle Weights and Dimensions Study. The vehicle was designated an additional vehicle by the study.

The vehicle was subjected to turning, air brake system, lateral/directional and roll stability, and trailer sway tests. A demonstration of straight-line braking was also conducted. Tests were conducted with the empty vehicle on a low-friction surface and the loaded vehicle on a high-friction surface.

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1/ INTRODUCTION

The effects of changes in truck weight and dimension parameters on combination vehicle stability and handling and on pavement response to axle group loading are being examined in the CCMTA/RTAC Vehicle Weights and Dimensions Study. The vehicle portion of the study involved both computer simulation of vehicle dynamic manoeuvres and testing of vehicles and components. Combination vehicles were classified into six families, based on the number of trailers and methods of hitching. A representative of each family was designated as the baseline vehicle configuration for that family. Additional vehicle configurations of interest were also defined. All baseline and additional vehicle configurations were tested to assemble a body of technical and visual data that described the stability and control characteristics of the vehicles with respect to certain performance measures.

The Ontario Ministry of Transportation and Communications (MTC) was asked to test the six baseline vehicles and three additional tractor-trailer combinations, as part of its contribution to the study. This report presents the results of a test of a 6-axle 48 ft (14.63 m) semitrailer combination, which is one of the additional vehicles. It refers frequently to a report describing procedures and equipment common to tests of all nine vehicles undertaken by MTC [1]. Similar reports present details of the tests of the other eight vehicles [2-9], and a summary report presents the results of tests of all six baseline vehicles [10]. A computer simulation of vehicle responses to actual test inputs using estimated vehicle data has also been conducted [11].

2/ TEST VEHICLE DESCRIPTION

The test vehicle consisted of the MTC Freightliner [1] and a single 48 ft (14.63 m) 3-axle flatbed semitrailer. The combination is typical of equipment used in Central Canada, where trailers with a widespread tandem axle and an airlift belly axle are permitted additional weight. The same combination was also tested concurrently as a 5- and 7-axle vehicle [8,9].

The equipment for these tests was obtained from the Roads and Transportation Association of Canada (RTAC). No modifications were made to the trailer except for purposes of attachment of test equipment, which had no effect on the operation of the vehicle, though unit weights and polar moments of inertia were affected.

The trailer was manufactured by Fruehauf in July 1984 and was a 48 ft (14.63 m) flatbed semitrailer with two fixed and two airlift axles, one of which was raised for these tests. It was model number PBX4W48102 and bore the serial number 2H8P04843ER033601.

The trailer had a nominal length of 14.63 m (48 ft) and a nominal width of 2.59 m (102 in). The trailer suspension comprised a Reyco four-spring leaf suspension system with long equalizer arms on the fixed axles and a Neway air suspension system for the two airlift axles. The axle spacings were 2.74 and 2.77 m (108 and 109 in). The spring centre width was 0.96 m (38 in), for the fixed axles, and 0.76 m (30 in) for the airlift axles. The airlift axles had shock abosorbers in parallel with the air springs, with a spacing of 0.30 m (12 in). The track width was 2.44 m (96 in). The vehicle overall length was 18.69 m (61.32 ft). The trailer was rated at 9620 kg/axle (21 164 lb/axle).

The trailer was fitted with new Michelin XZA radial tires, in load range H and size 11R22.5. These tires were run a nominal distance of 160 km (100 mi) before any testing and were then, subsequently, used for all tests. Tire pressure was set cold at 689 kPa (100 psi), which is the manufacturer's recommended value for full load. This was used for all tests and represents the common operating practice of not reducing tire pressure when running empty.

The test vehicle is shown in Figure 1, in test condition with outriggers installed. The dimensions of the test vehicle are presented in Figure 2. Empty weight of the combination in test condition was 22 594 kg

(49 710 lb). Concrete blocks were used to obtain a loaded weight of 41 543 kg (91 390 lb). Airlift axle pressure was 159 kPa (23 psi) for the empty vehicle and 345 kPa (50 psi) loaded. Axle loads in these conditions are given in Table 1.

Table 1/ Axle Loads

Axle No.	Empty		Loaded	
	(kg)	(lb)	(kg)	(lb)
1	4 918	10 820	5 373	11 820
2	4 554	10 019	7 505	16 510
3	4 554	10 019	6 809	14 980
4	2 856	6 284	7 396	16 270
5	2 856	6 284	7 714	16 970
6	2 856	6 284	6 746	14 840
Total	22 594	49 710	41 543	91 390

The empty weight exceeds that which would normally be seen on the highway, because the tractor is considerably heavier than late-model equipment, because of the lifted axle, and because of the weight of test equipment installed, particularly the outriggers. A target axle load of 8000 kg (17 600 lb) was set for all axles except for the steer axle. This was nearly attained, with the exception of the tractor drive axles. The legal gross weight of the vehicle tested is about 50 000 kg (110 000 lb) in Ontario and Quebec, and 47 700 kg (105 000 lb) in B.C., where the belly axle is required to be steerable.

The height of the centre of gravity of the empty trailer sprung mass was estimated as 0.30 m (11.8 in) below the top of the floor. The centre of gravity height was estimated as 0.23 m (9 in) above the top of the floor in the loaded condition.

3/ TEST PROGRAM

3.1/ Test Procedures

The test vehicle was prepared for testing in the following way:

1/ A mechanical inspection was carried out, and any necessary repairs or maintenance was done.
2/ Outrigger and safety cable attachments and load block retention sills were installed on the trailer.
3/ Outriggers were installed on the trailer.
4/ The boxes containing instrument packages, power supplies and signal conditioning, other instruments, and cabling were installed.
5/ New tires were installed, and pressures were set.
6/ Other fittings necessary for testing were installed.
7/ Concrete blocks were located on the trailer bed to achieve specified axle loads.
8/ Notes were made from detailed physical inspection, including an inventory of components and measurement of dimensions.
9/ The MTC tractor was coupled to the trailer.
10/ The combination vehicle was weighed, empty and loaded.
11/ A functional test of the on-board electronics was conducted.
12/ Test runs were made to shake down the vehicle instrumentation and familiarize the test driver with the vehicle's handling characteristics.
13/ Tires were run a nominal distance of 160 km (100 mi).
14/ Articulation angle between the tractor and trailer was calibrated.
15/ Photographs and video film were taken to record details of the vehicle and test equipment.

The following tests were performed:

- Offtracking
- Right-hand turn
- Channelized right turn
- Air brake system
- Straight-line braking, empty vehicle, low-friction surface
- Evasive manoeuvre, empty vehicle, low-friction surface
- Sinusoidal steer, loaded vehicle, high-friction surface
- Lane change, loaded vehicle, high-friction surface
- Normal straight-line driving
- Steady circular turn, loaded vehicle, high-friction surface

All tests followed standard procedures [1], except as noted.

3.2/ Instrumentation

The instrumentation shown in Table 2 was installed. Brake pressure transducers were only installed in the trailer for the air brake system test, but all other instrumentation was installed for all tests. Data were always captured from all instrumentation, but only those pertinent to a particular test were analysed.

Tractor instruments were selected from the instrumentation that is permanently installed on the tractor. Instruments for the trailer were mounted in a box placed on the trailer deck, which also contained power supplies and signal conditioning. Trailer lateral acceleration and roll angle were measured at a point midway between the kingpin and axle.

Full details of the instrumentation, signal conditioning, and data capture system are presented elsewhere [1].

3.3/ Data Capture and Data Processing

Data were digitized on board the vehicle and transmitted by telemetry as a pulse-code modulated (PCM) data stream to a ground station, where they were recorded on magnetic tape and captured in real time by an HP-1000 computer system. Test data for a run were processed immediately after the run, and results from a series of runs were subsequently analysed using the computer system [1].

Many test runs of all types were conducted for this vehicle. Not all these runs were used in the preparation of this report. In a number of instances, a run failed to meet a test condition, or runs were made to evaluate the ability of the vehicle to make a particular manoeuvre.

Table 2/ Instrumentation Installed

No	Measurement	Instrument	Full Scale
1	Tractor steer angle	Spectrol 139 potentiometer	25.02°
2	Tractor roll angle	Humphrey CF18-0907-1 gyro package	8.85°
3	Tractor lateral acceleration	Kistler 303B accelerometer	0.957 g
4	Tractor yaw rate	Humphrey RT03-0502-1 angular rate transducer	38.7°/s
5	Tractor longitudinal acceleration	Kistler 303B accelerometer	0.974 g
6	Tractor speed, axle 1 right	Airpax 087-304-0044 zero velocity magnetic pickup	104.8 km/h
7	Tractor distance, axle 1 right	Airpax 087-304-0044 zero velocity magnetic pickup	56.3 m/ramp
8	Tractor fifth wheel load, left-hand side	MTC load cell	9890 lb
9	Tractor fifth wheel load right-hand side	MTC load cell	10290 lb
10	Tractor treadle valve pressure	Celesco PLC-200G	100 psi
11	Tractor brake pressure, axle 2 Left	Celesco PLC-200G	99.80 psi
12	Tractor lateral acceleration at fifth wheel	Columbia SA-107 accelerometer	0.996 g
13	Tractor yaw angle	Humphrey CF18-0907-1 gyro package	17.73°
14	Trailer 1 articulation angle	Celesco pull cord DV-301-150	19.792°
15	Trailer 1 lateral acceleration	Columbia SA-107 accelerometer	0.995 g
16	Trailer 1 roll angle	Humphrey VM02-0128-1 vertical gyro	8.90°
17	Trailer 1 outrigger touchdown	Strain gauge bridge	1.0 V
18	Dolly 1 hitch angle	Spectrol 139 potentiometer	25.0°
19	Dolly 1 lateral acceleration	Columbia SA-107 accelerometer	0.996 g
20	Brake pressure, axle 4 right	Celesco PLC-200G	104.96 psi
21	Brake pressure, axle 5 right	Celesco PLC-200G	101.06 psi
22	Brake pressure, axle 6 right	Celesco PLC-200G	102.07 psi

4/ RESULTS

4.1/ Offtracking

Steady-state offtracking is considered an indicator of vehicle turning ability. Offtracking of the vehicle was evaluated by making a complete turn around a circle of radius 29.87 m (98 ft). The vehicle outer wheel tracked the inside of the circle. Turns were made in both directions, as shown in Figure 3. At the end of a turn, the vehicle was parked and the radius to each axle was measured, according to the standard test procedure [1].

The results are shown in Table 3. The measured data were averaged for the left and right turn and then compared to data generated by a simple offtracking formula [12]. The difference between actual and computed values shown in the last column of Table 3 is so small that steady-state offtracking can clearly be estimated very accurately by this simple formula.

The final offtracking for the counter-clockwise turn is shown in Figure 4. After averaging for both directions and correcting for differences in axle track width, the offtracking of 2.41 m (7.9 ft), shown in Figure 4, became 2.38 m (7.8 ft).

Table 3/ Offtracking

Axle No.	Track Width (m)	Radius to Inner Wheel		Difference (m)	Average (m)	Calculated (m)	Difference %
		Right Turn (m)	Left Turn (m)				
1	2.31	27.56	27.45	0.11	27.51	27.56	+0.18
2	2.37	27.31	27.30	0.01	27.31	27.21	-0.37
3	2.37	27.28	27.33	0.05	27.31	27.21	-0.37
4	2.37	25.40	25.49	0.09	25.45	25.45	0.0
5	2.37	25.12	25.15	0.03	25.14	25.30	+0.63
6	2.37	25.11	25.13	0.02	25.12	25.45	+1.30

4.2/ Right-Hand Turn

A 90° right-hand turn is a very demanding manoeuvre for a large truck. The vehicle's swept path in a 90° right-hand turn of 15 m (49.2 ft) radius was measured, according to the standard test procedure [1]. This radius is typical in an urban area or where there is limited truck

traffic. The swept path is shown in Figure 5.

The vehicle is shown in Figure 6 during the turn, at a point close to its maximum excursion out of the exit lane. The maximum excursion out of lane was 0.7 m (2.29 ft). It was out of the exit lane for a distance of 21.0 m (68.9 ft), as derived from Figure 5. This test was conducted at a creep speed and represents about the best possible turn. A rolling turn would probably result in a greater excursion out of the exit lane.

4.3/ Channelized Right Turn

The vehicle's swept path in a channelized right turn was measured according to the standard test procedure [1].

The vehicle is shown during the turn in Figure 7. The clearance of the innermost wheel of the rear trailer's rear axle from the inner curb is shown in Figure 8 as a function of distance through the curve. The minimum clearance was only 1.12 m (44 in) in the 5.5 m (18 ft) wide roadway.

The roadway geometry used for this test is typical of an urban area, where space is limited. The curb radius was 25 m (82 ft), and entry and exit tapers typical of four-lane roadways with a 60 km/h speed limit were used. The vehicle was driven with the left front wheel tracking the curb. In practice, a driver would allow some clearance on his side, if only to stay clear of catch basins. This would mean the rear axle would come close to the inner curb.

4.4/ Air Brake System

The air brake system of the combination was evaluated according to standard test procedure [1].

The trailer air brake system was inspected. A schematic of the system is shown in Figure 9. All slack adjusters required manual adjustment. Stroke was adjusted to the minimum, about 32 mm (1.25 in) on each axle. The tractor was supplied with shop air, regulated at 689 kPa (100 psi).

The SAE J982a style test was performed, and the results, presented in Table 4, are the average of several tests, each with a time resolution of 0.02 s. The application and release times of this test are typical of those obtained from tests conducted on other similar combinations. A typical time history response of application and release is presented in

Figure 10.

Table 4/ Air Brake Timing, SAE J982a Style Test

Location	Application Timing 0-60 psi (s)	Release Timing to 5 psi (s)	Final Pressure (psi)
Treadle	0.03	0.18	92.5
Axle 2	0.36	0.56	90.9
Axle 4	0.43	0.91	87.7
Axle 5	0.43	0.95	86.2

4.5/ Straight-Line Braking

It is difficult to conduct rigorous braking tests and achieve consistent results. A demonstration of modes of instability of the combination vehicle in straight-line braking was, therefore, conducted. A series of runs was made with the empty vehicle approaching the low-friction test area at 47 km/h and the driver braking using the treadle valve. Runs were made using various application pressures, to the point where groups of wheels locked. The driver was instructed not to attempt to counter any loss of control, except as necessary to avoid hazard. The standard test procedure was followed. Note that the airlift axle was lowered for this test, even though it would be raised in normal operation on the highway when the vehicle was empty.

The vehicle combination was evaluated primarily in terms of the yaw response of vehicle units, which is the heading angle of the vehicle unit (in degrees), with zero parallel to the original direction of travel. Any significant yaw seen in this manoeuvre arose from lateral/directional instability of a vehicle unit.

The time history of a typical run that resulted in loss of control is shown in Figure 11. The initial average brake application of about 276 kPa (40 psi) caused all braked wheels to lock, the tractor jackknifed to the left, the safety cables were engaged (as seen from the 15° limit on articulation angle), and the vehicle rotated as a unit. The tractor heading reached the limit of the signal conditioning system. If the tractor front axle brakes had been used, the likelihood of a tractor jackknife would have been much reduced.

A summary of peak vehicle responses is shown in Figure 12, as a function of average treadle valve pressure. This shows that the tractor is on the verge of a jackknife at lower brake pressures and the jackknifing was in either direction.

4.6/ Evasive Manoeuvre

The object of this test was to evaluate empty vehicle lateral/directional characteristics at the limits of stability on a low-friction surface. A series of runs was made where the driver made an evasive manoeuvre, which is considered representative of a high-speed accident avoidance situation on a two-lane, two-way highway. The test used gates of 22.5 m (73.8 ft) for the lane change to the left and the return to the original lane, separated by 20 m (65.6 ft) in the left lane. Note that the airlift axle was also lowered for this test. The runs were made in accordance with the standard test procedure [1].

Data from this test were lost due to mechanical failure of the computer disk drive and were found to be unrecoverable from the backup tape. The following comments, therefore, are based upon notes, review of the video tapes, and computer summaries made during the test.

The vehicle's behaviour was predictably between that of the 5- and 7-axle combinations tested concurrently [8,9]. Data captured at the time of the test indicated that the tractor required increasing steer input to negotiate the manoeuvre as speed increased. This, coupled with observations of tractor slide and tire chatter, indicated that the tractor was showing signs of understeer. At the higher speeds, it was noted that key course markers were struck, indicating some loss of tractor directional control. Little sway was noted at the trailer.

4.7/ Sinusoidal Steer

The objective of this test was to evaluate characteristics of rearward amplification of lateral acceleration for this combination. A series of runs was made where the driver made a sinusoidal steer input to the vehicle while travelling at a steady speed, in accordance with the standard test procedure [1]. This test was conducted at speeds of 63, 84, and 94 km/h, with steer input periods between about 2 and 5 s. However, the data from runs at 63 and 84 km/h were lost due to mechanical failure of the computer's disk drive while the data were being archived on tape.

The vehicle combination was evaluated in terms of the lateral acceleration response of the trailer. Rearward amplification of lateral acceleration of the trailer is presented in Figure 13, as a function of tractor steer input period for the one test speed. This gain is defined as the peak-to-peak trailer lateral acceleration response divided by the peak-to-peak tractor lateral acceleration, and is dimensionless.

It is evident from Figure 13 that rearward amplification is somewhat sensitive to steer period reaching the highest value of about 0.92 at around 3 s. The results show that, at highway speed, this is a very stable vehicle, because of its low response to input. Figure 14 shows the response of a typical run for a steer period of about 2.76 s at 94 km/h.

4.8/ Lane Change

The objective of this test was to evaluate vehicle stability characteristics in a dynamic manoeuvre. A series of runs was made where the driver made a lane-change manoeuvre, which is considered representative of a high-speed accident avoidance situation on a four-lane or divided highway. The runs were made in accordance with the standard test procedure [1].

The test used a gate of 30 m (98.4 ft) for the lane change. This was used to provide a vehicle speed of about 80 km/h, which is a typical speed limit and might permit some comparison of the results of this test with that described in the preceding sections.

Unfortunately all data from this test were lost because of the mechanical failure of the computer's disk drive. The data were also not recoverable from the analog tape recorder because of errors on the tape. The following comments, therefore, are based on notes, review of the tapes, and video and computer summaries made during the test.

The vehicle's behaviour was predictably between that of the 5- and 7-axle combinations tested concurrently [8,9]. It remained stable up to the maximum test speed of 94 km/h. Overshoot appeared evident but within lane boundaries, some of which was, no doubt, due to driver steer corrections in the exit lane, as shown in Figure 15. Roll amplitudes appeared somewhat less than for the 7-axle semi [9] but greater than for the 5-axle vehicle [8].

4.9/ Normal Straight-Line Driving

The objective of this test was to attempt to evaluate lateral motion of the rear trailer of the combination, the phenomenon known as trailer sway. A series of runs was made with the loaded vehicle driven normally at 94 km/h in a straight line, according to the standard test procedure [1].

As previously mentioned, the vehicle was very stable and, if any slight steer corrections made in the course of normal driving, and roughness of the test track surface, resulted in trailer sway, it was not readily perceptible to the occupants of a chase vehicle. Root mean square (RMS) lateral acceleration of the rear trailer was 0.99 g/° of RMS steer input.

4.10/ Steady Circular Turn

The objective of this test was to evaluate vehicle steady-state rollover characteristics to determine the high-speed offtracking of the vehicle and examine the side loads exerted on the tractor by the trailers. A series of runs was made with the vehicle circumscribing a circle with a 50 m (164 ft) radius at a steady speed, according to the standard test procedure [1].

The results of this test are summarized in Figure 17. The vehicle combination was evaluated primarily in terms of the roll response of the vehicle units. Average steady-state roll angle, presented in Figure 17 as a function of tractor lateral acceleration, increased with speed. Average steady-state articulation angle decreased modestly with increase in lateral acceleration, and as a consequence, the offtracking decreased. The lateral force experienced by the tractor fifth wheel is also shown in Figure 17, as a function of tractor lateral acceleration. This shows a gradient of 58.9 kN/g (13 200 lb/g).

At the limiting speed of 63 km/h, a lateral acceleration of 0.53 g, the outrigger touched down, around 8 s in Figure 18, and the trailer swung out around 9 s, relieving the lateral acceleration on the trailer and reducing the articulation angle. This is also shown in Figure 19. It is possible the vehicle would not have rolled over. This manoeuvre at the high lateral acceleration required a very high effort on the part of the driver just to follow the circle.

A tilt test was conducted on this vehicle as part of a separate test program [14]. The high-side wheels of the rear trailer lifted at a tilt angle of 29.3°, after all corrections were made, which corresponds to a lateral acceleration of 0.56 g. This is in quite good agreement with the rear trailer's lateral acceleration at outrigger touchdown of 0.53 g. A full discussion of the tilt test is presented elsewhere [14].

5/ DISCUSSION

Tests were conducted with the equipment as provided. No efforts were made to modify the equipment, except as required for testing, and these modifications did not affect vehicle operation.

Tests were conducted in various weather conditions. Tires wore progressively as the various tests were conducted, particularly those on the right-hand wheel of the rear axle. The tests on this vehicle followed those of the 5-axle 48 ft (14.63 m) semi [8], and the steady circular turn was clearly causing severe wear on the outer edge of this tire. The outrigger assembly was additional to normal trailer equipment, and the characteristics of the trailers were, therefore, somewhat atypical, at least in the empty condition.

It is not possible to make any meaningful remarks on the effect these factors might have had on the results. The results presented pertain to the particular vehicle tested, and results different in some respects might be obtained for another vehicle at another time.

This vehicle was considered an easy vehicle to drive by the test driver. It tracked well but required more effort to manoeuvre than either the 5-axle 45 ft (13.72 m) semi [2] or the 5-axle 48 ft (14.63 m) semi [8], because of the lowered airlift axle. It did, however, require a little less space to manoeuvre than these vehicles. It exhibited high stability in all dynamic manoeuvres. However, the trailer centre of gravity was quite low -- about 1.73 m (68 in) from the ground. The centre of gravity for some loads can result in a trailer centre of gravity 2.5 m (100 in) or more from the ground, which would reduce the rollover threshold to somewhere around 0.3 g [15]. The lane change would then likely have resulted in rollover at some speed less than 95 km/h.

6/ CONCLUSIONS

A 6-axle tractor semitrailer combination was tested by the Ontario Ministry of Transportation and Communications, as part of the CCMTA/RTAC Vehicle Weights and Dimensions Study. The vehicle was designated as of particular interest by the study.

The vehicle was subjected to turning, air brake system, lateral/directional and roll stability, and trailer sway tests. A demonstration of straight-line braking was also conducted. Tests were conducted with an empty vehicle on a low-friction surface and a loaded vehicle on high-friction surface.

The length of this vehicle clearly contributed to the significant space required to make turns, though it required less space than a comparable 5-axle semi.

The air brake system was relatively fast and well balanced.

The lateral/directional stability of the vehicle was excellent, both empty on a low-friction surface and loaded on a high-friction surface. Stability varied little with speed up to 100 km/h. The roll stability was very high, primarily because the trailer centre of gravity was low. A higher centre of gravity would significantly reduce the rollover threshold.

7/ REFERENCES

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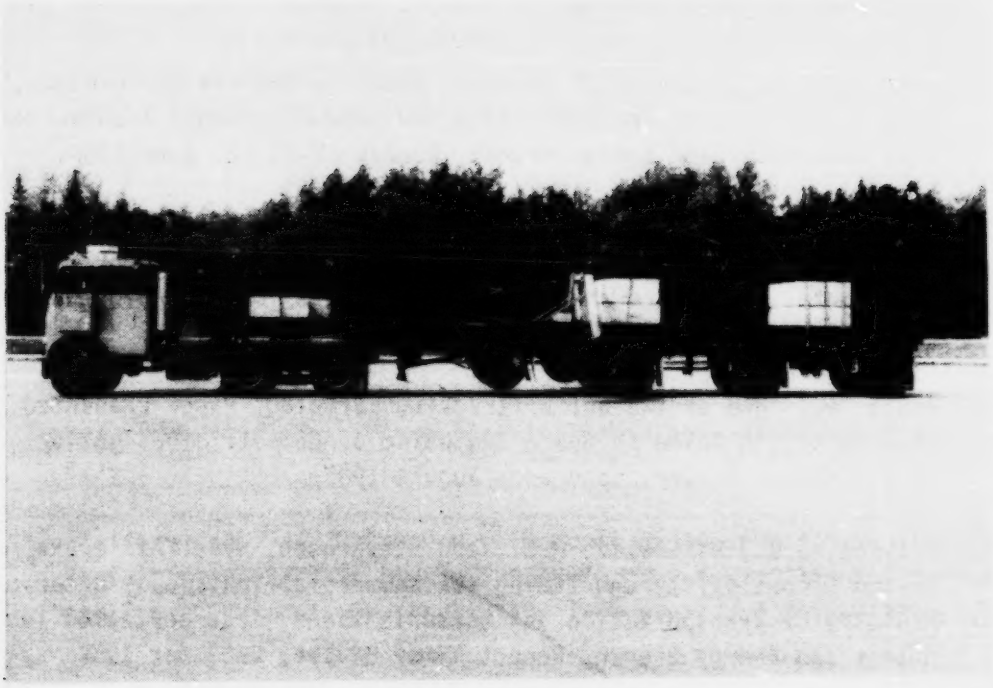


Figure 1/ 6-Axle 48 ft Semi, View of Vehicle

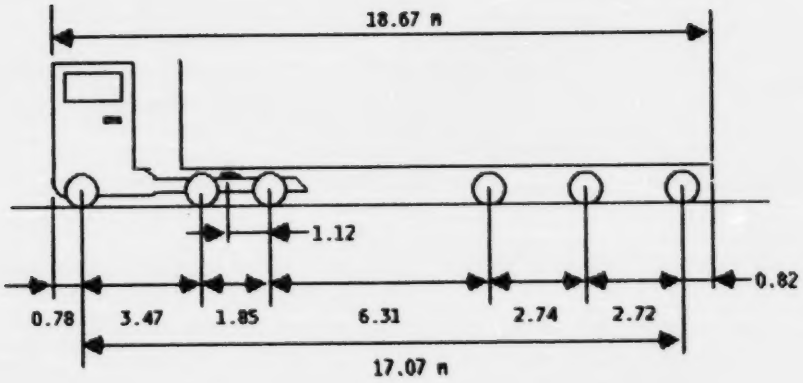


Figure 2/ 6-Axle 48 ft Semi, Vehicle Dimensions

Figure 3/ 6-Axle 48 ft Semi,
Offtracking

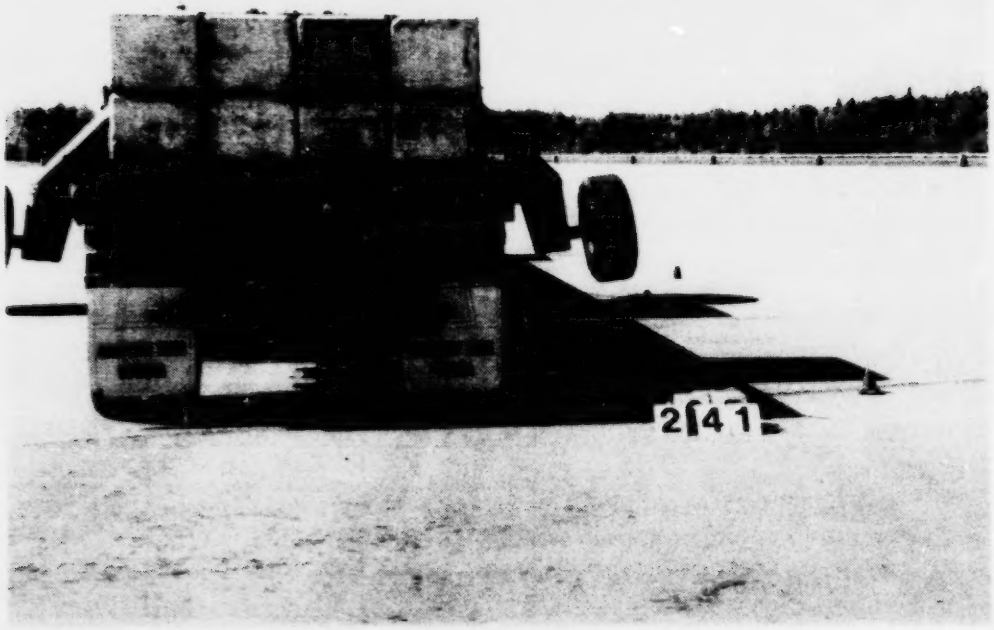
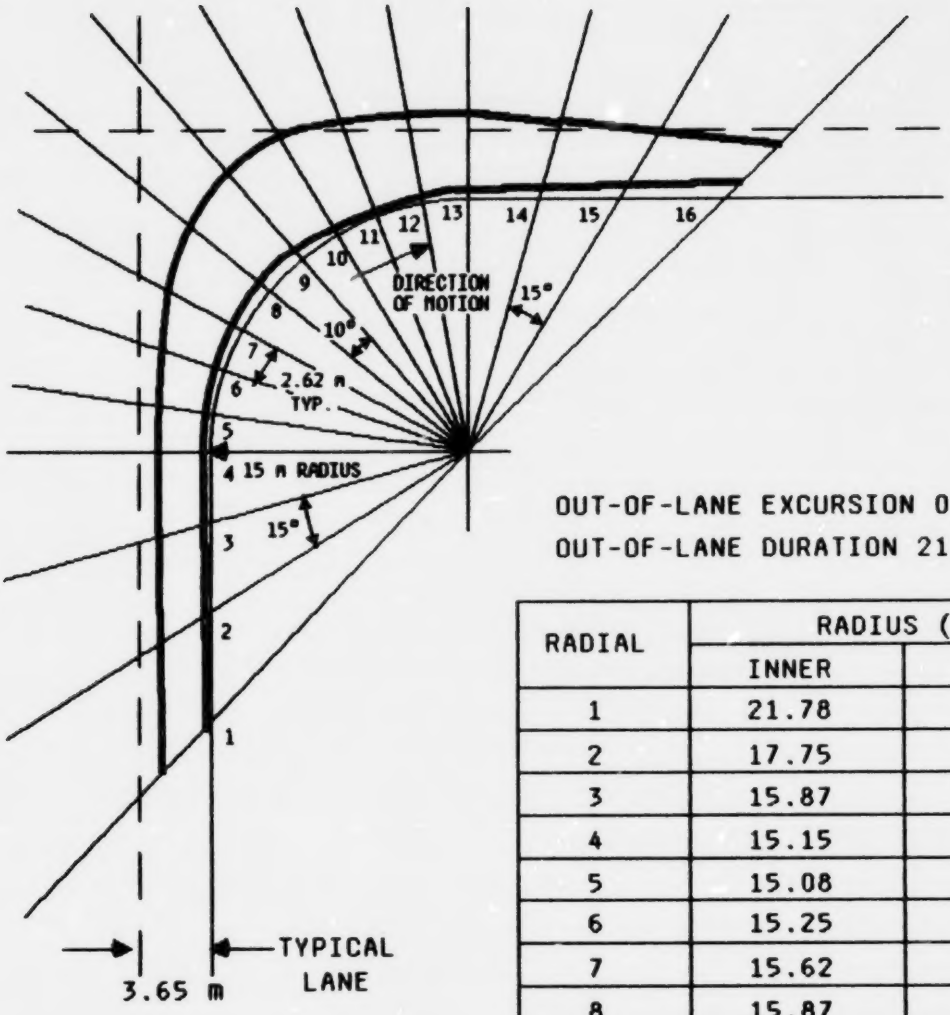


Figure 4/ 6-Axle 48 ft Semi,
Counter-Clockwise Final Offtracking



OUT-OF-LANE EXCURSION 0.7 m

OUT-OF-LANE DURATION 21 m

RADIAL	RADIUS (m)	
	INNER	OUTER
1	21.78	-
2	17.75	-
3	15.87	-
4	15.15	17.75
5	15.08	17.82
6	15.25	18.54
7	15.62	19.62
8	15.87	20.51
9	15.54	21.20
10	15.21	21.56
11	15.07	20.58
12	15.09	19.76
13	15.40	19.54
14	16.47	20.17
15	18.48	-
16	22.40	25.96

Figure 5/ 6-Axle 48 ft Semi, Right-Hand Turn Swept Path

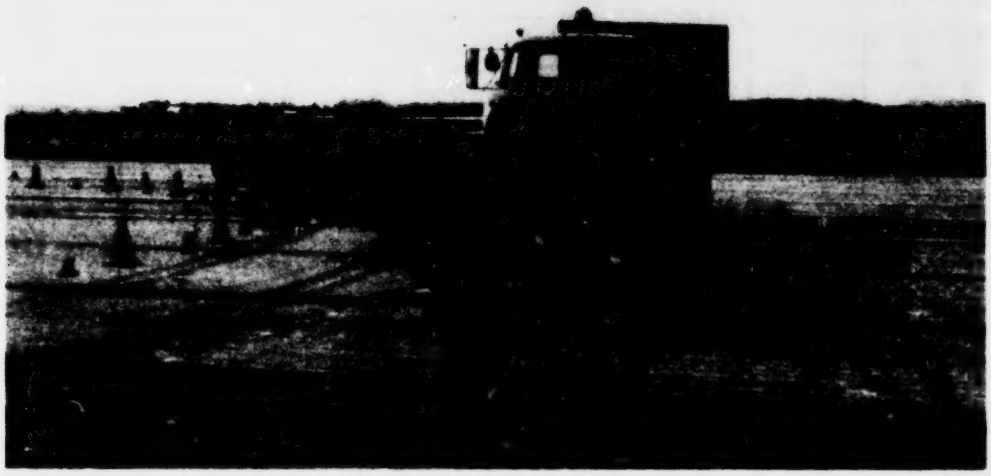


Figure 6/ 6-Axle 48 ft Semi, Right-Hand Turn

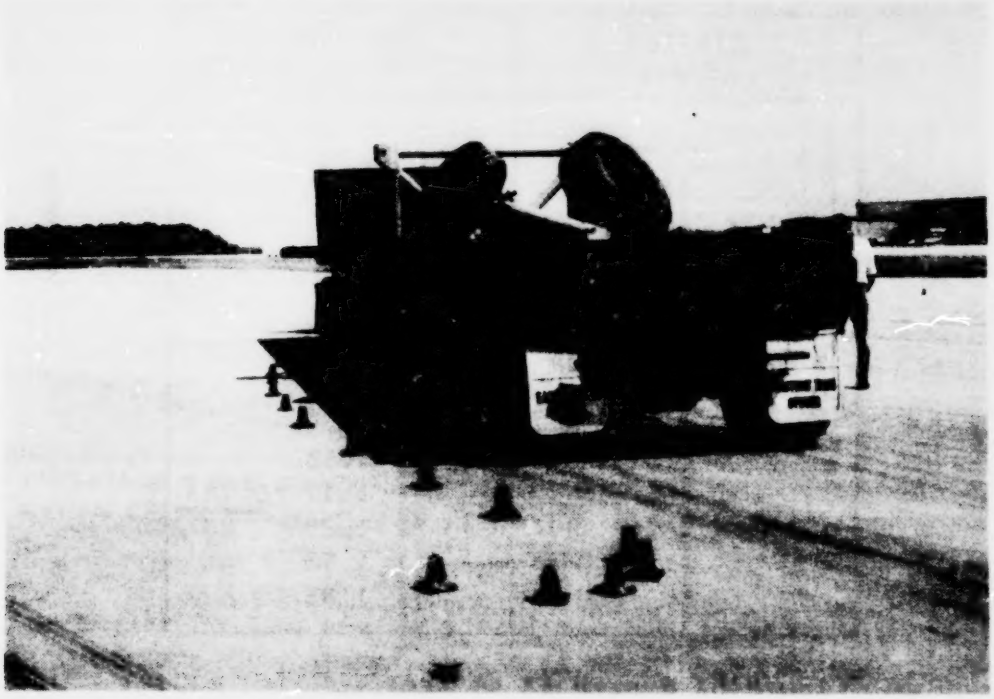
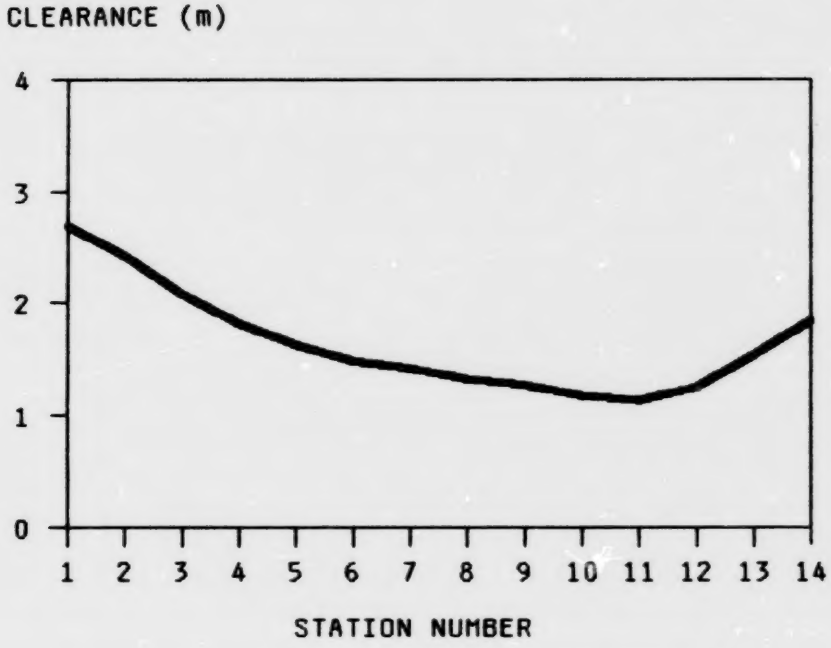


Figure 7/ 6-Axle 48 ft Semi, Channelized Right Turn



STATION NUMBER	CLEARANCE (m)
1	2.70
2	2.44
3	2.07
4	1.81
5	1.62
6	1.48
7	1.40
8	1.32
9	1.26
10	1.18
11	1.12 *(LOW)
12	1.25
13	1.53
14	1.85

**Figure 8/ 6-Axle 48 ft Semi,
Channelized Right-Turn
Clearance from Inner Curb**

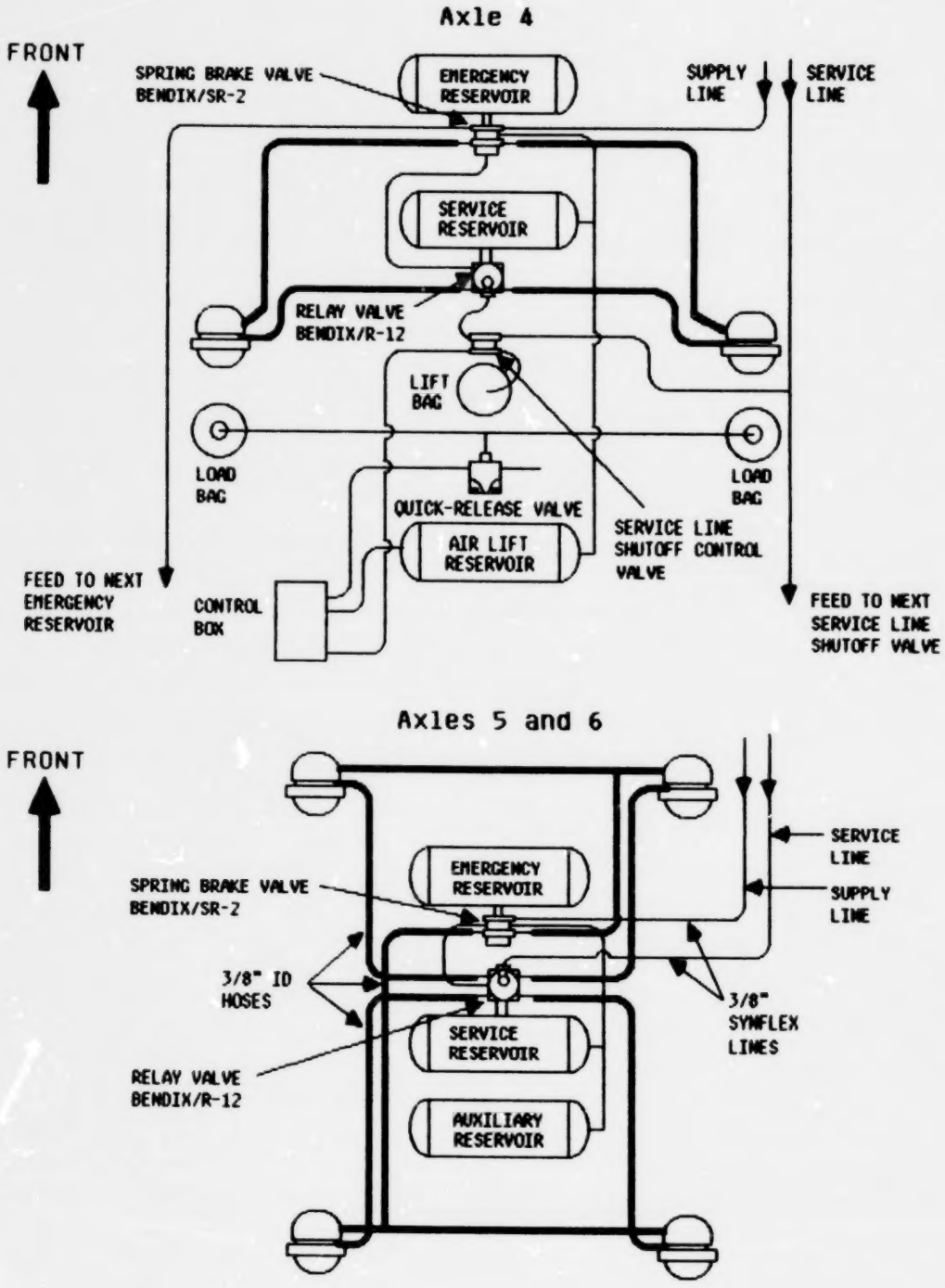


Figure 9/ 6-Axle 48 ft Semi,
Air Brake System Schematic

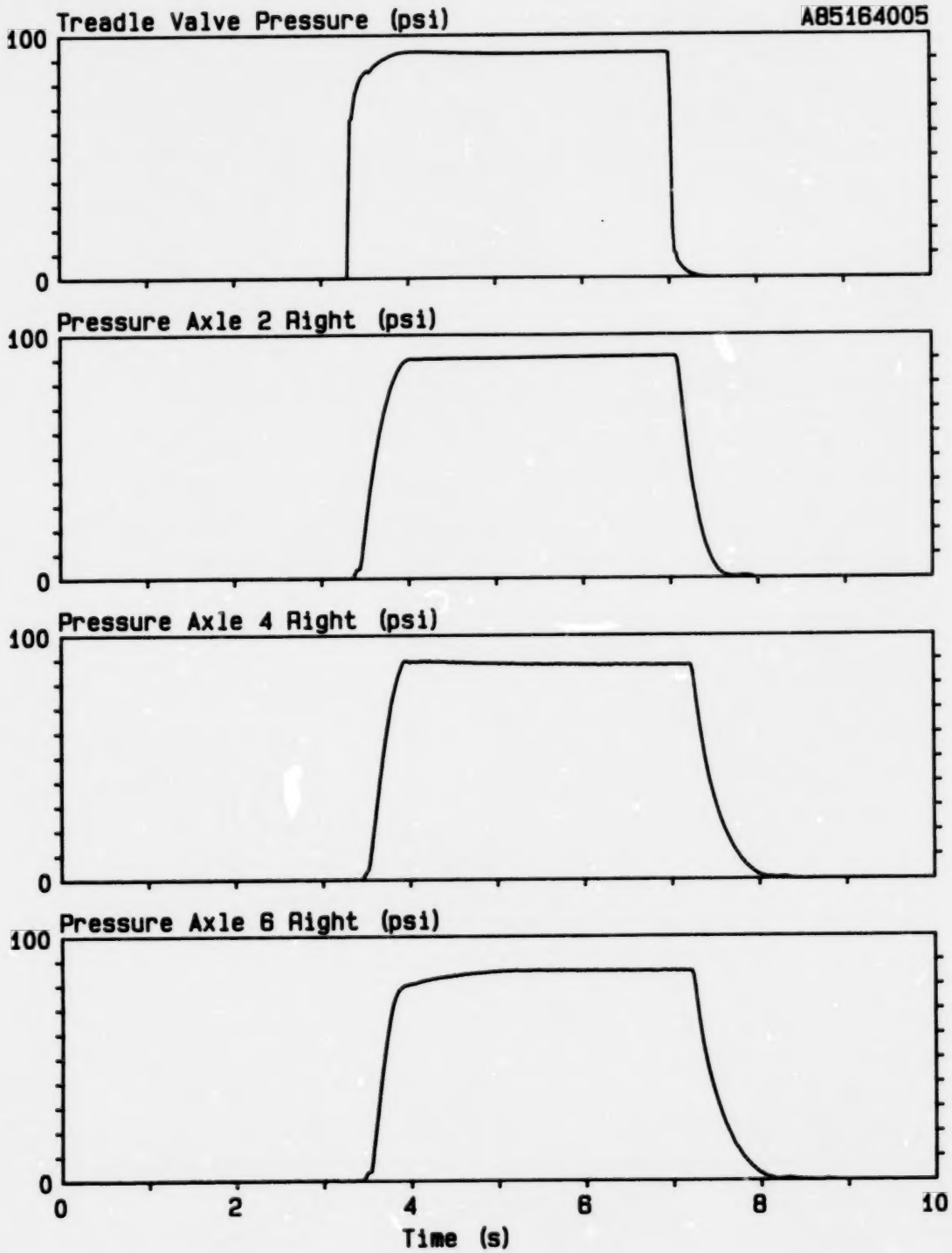


Figure 10/ 6-Axle 48 ft Semi,

Air Brake Application and Release

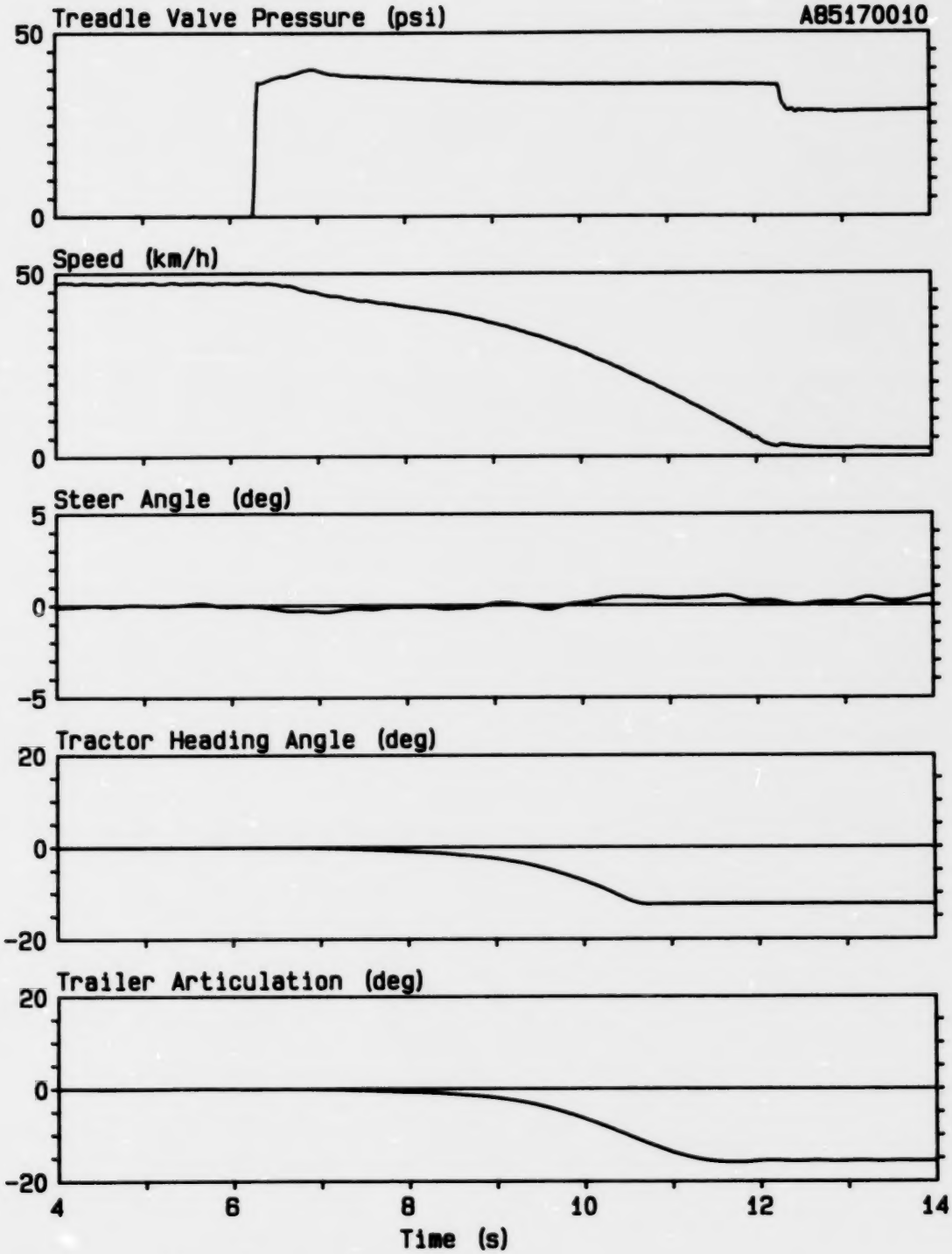


Figure 11/ 6-Axle 48 ft Semi,

Vehicle Response to Straight-Line Braking

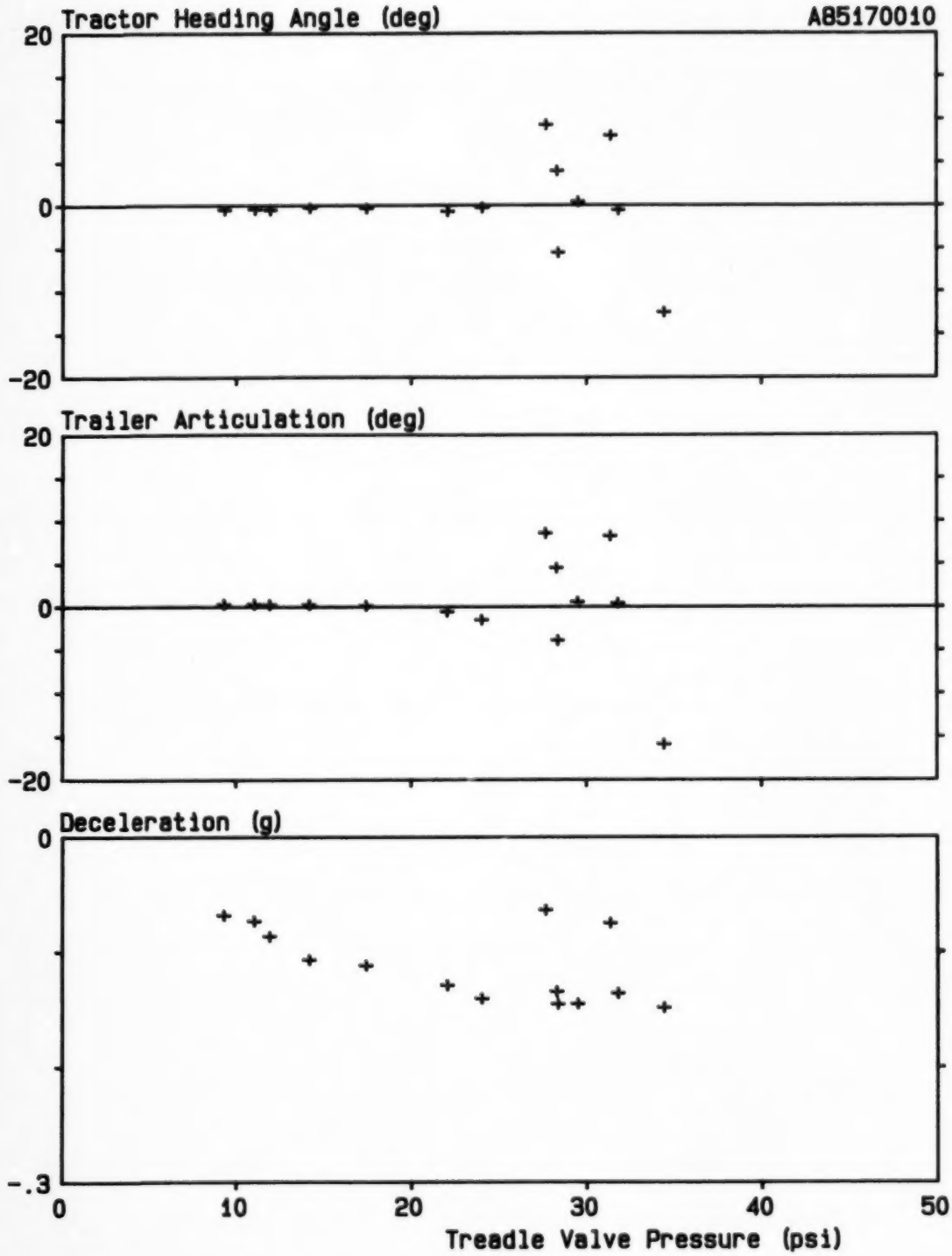


Figure 12/ 6-Axle 48 ft Semi, Straight-Line Braking Responses vs Treadle Valve Pressure

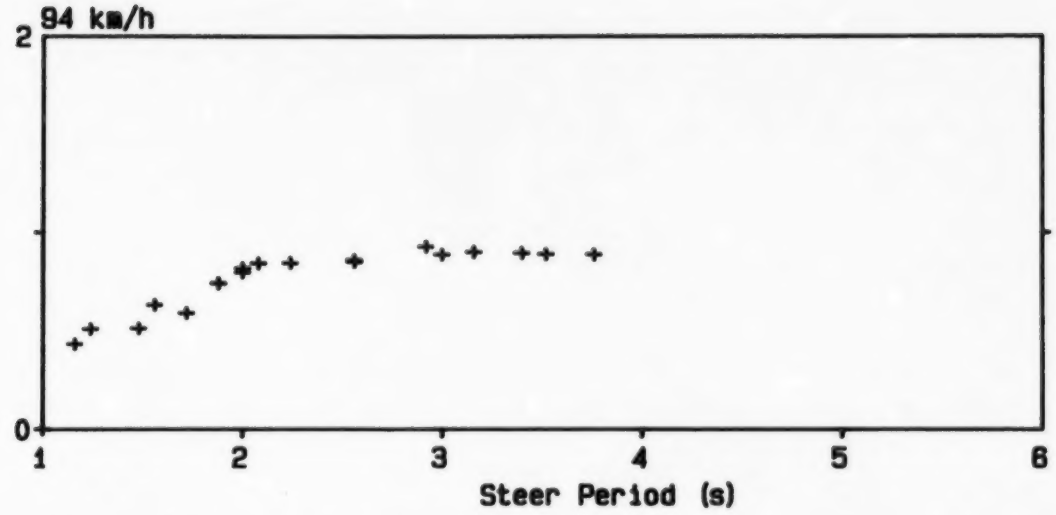


Figure 13/ 8-Axle 48 ft Semi,

Rearward Amplification of Lateral Acceleration

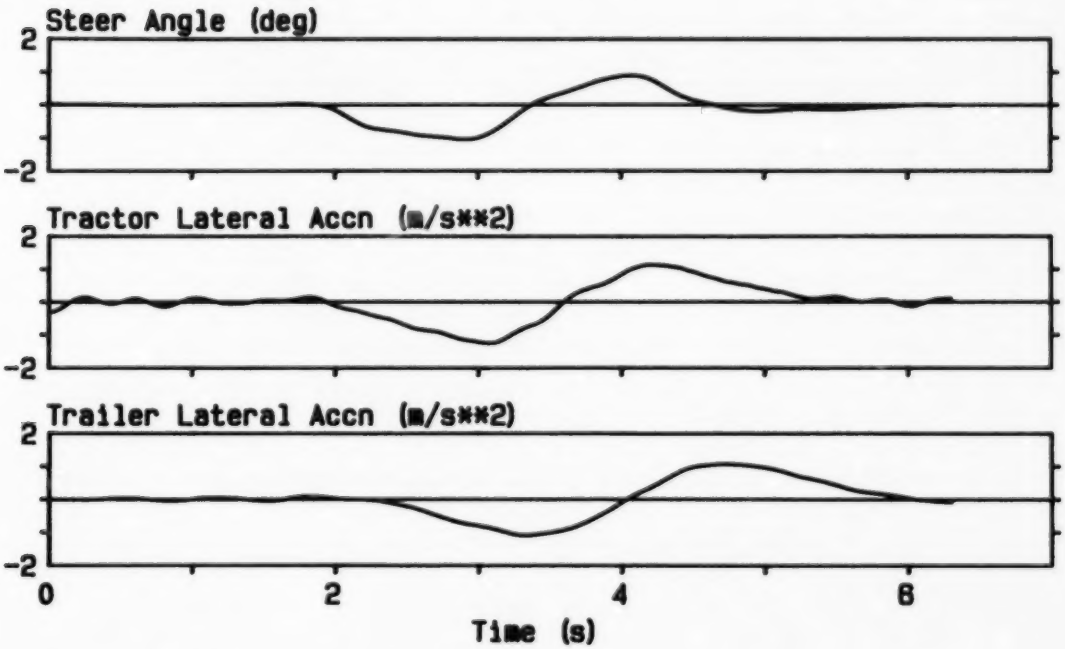


Figure 14/ 8-Axle 48 ft Semi,

Vehicle Response to Sinusoidal Steer at 94 km/h

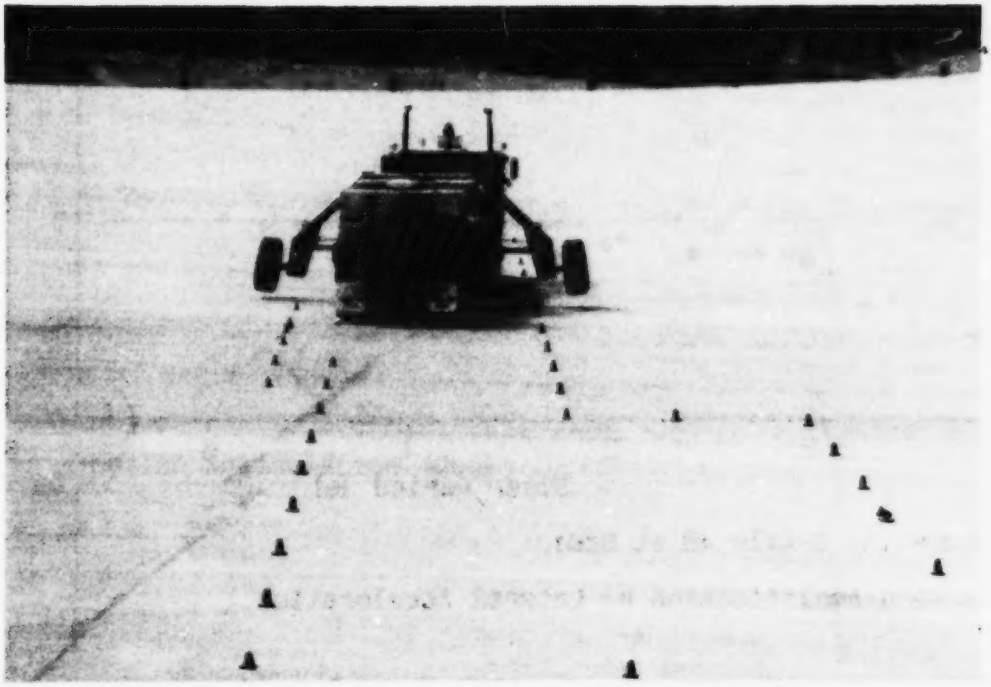


Figure 15/ 6-Axle 48 ft Semi Making Lane Change

Figure 16/ 6-Axle 48 ft Semi Making Lane Change

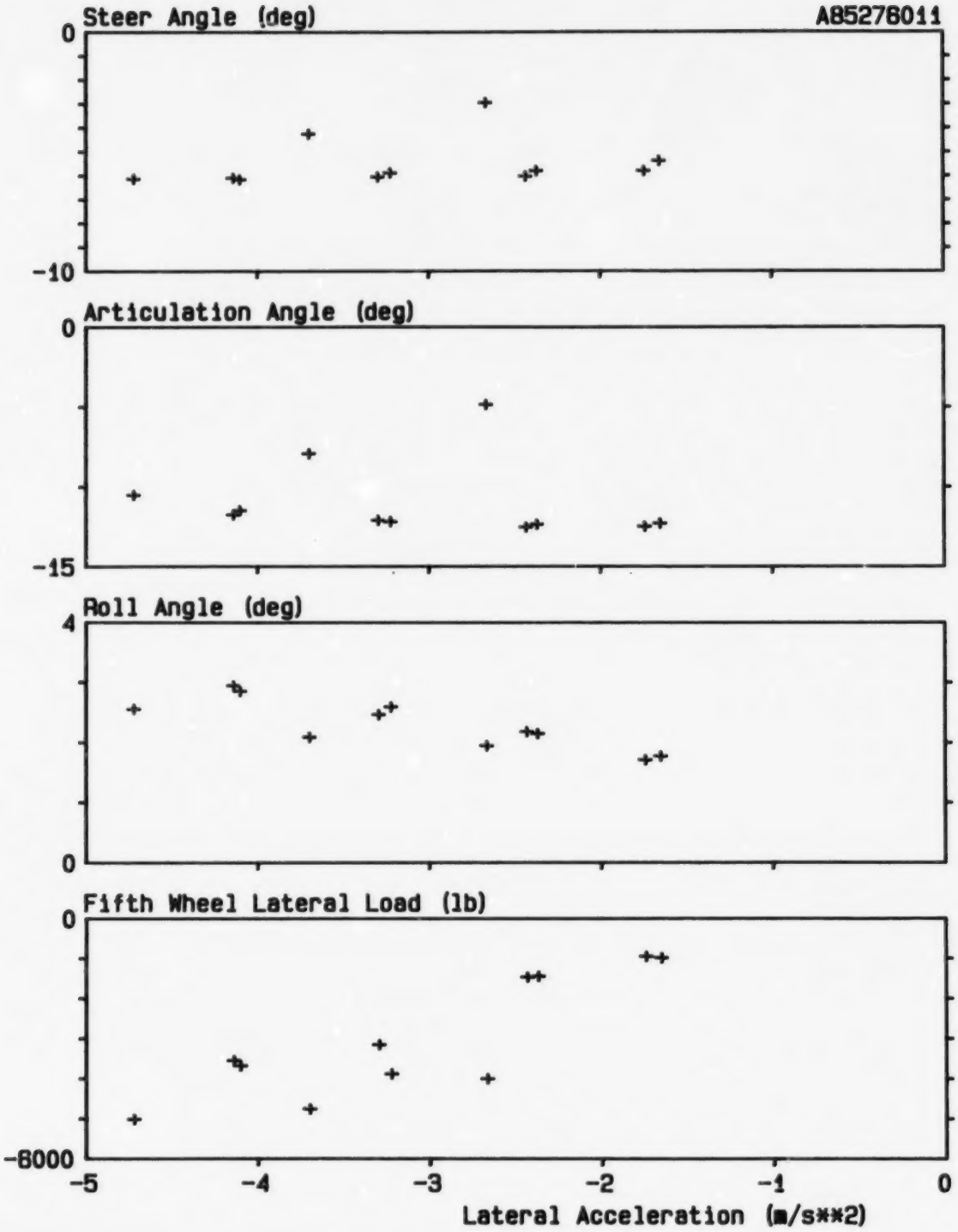


Figure 17/ 6-Axle 48 ft Semi, Steady Circular Turn, Vehicle Responses vs Tractor Lateral Acceleration

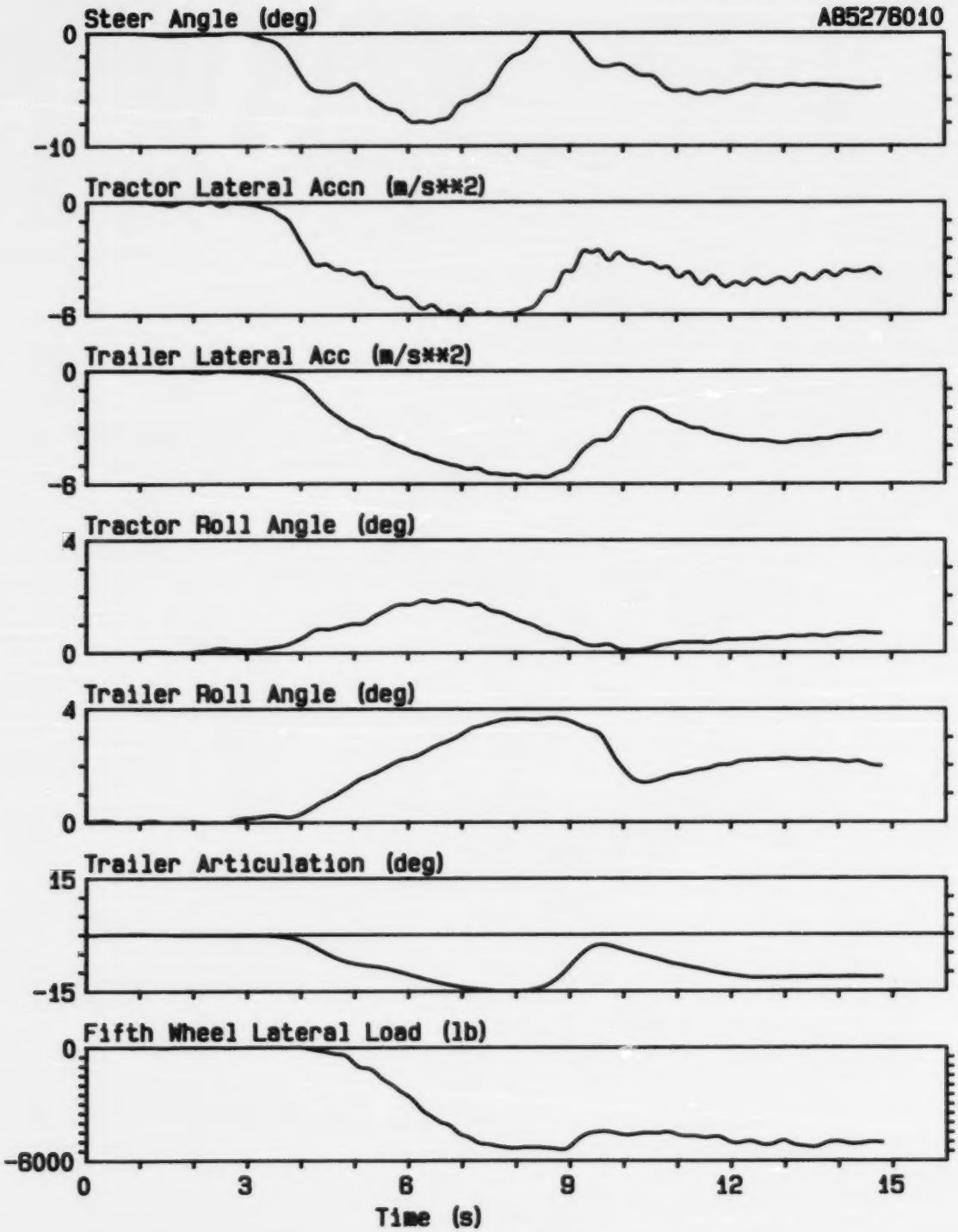


Figure 18/ 6-Axle 48 ft Semi, Steady Circular Turn, Vehicle Responses at 63 km/h

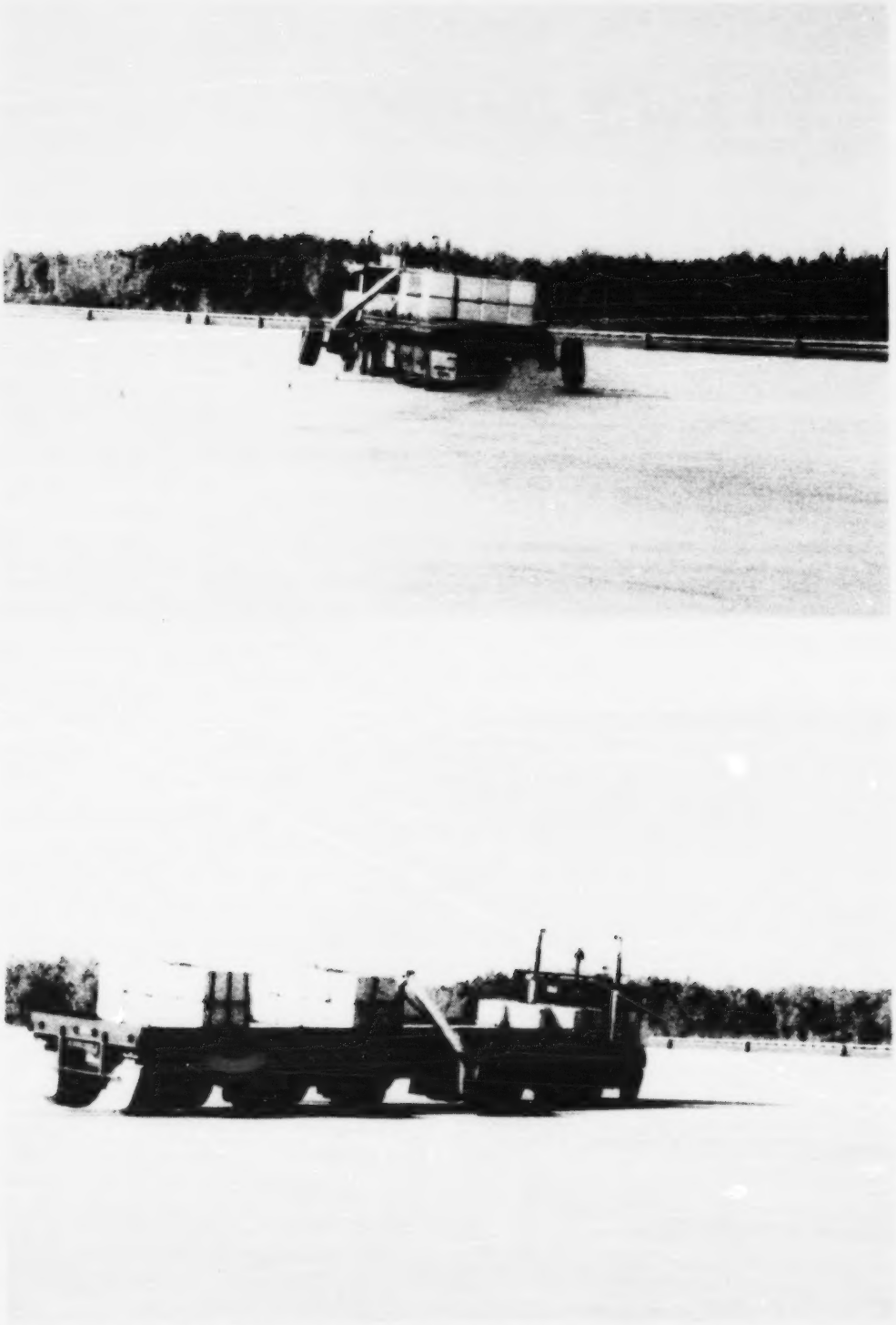


Figure 19/ 6-Axle 48 ft Semi Making Steady Circular Turn